



## Dynamic and control of an absorber - desorber plant Case study of the Heilbronn plant

Octavius CCS Conference 17-19 November 2015

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# Background and motivation

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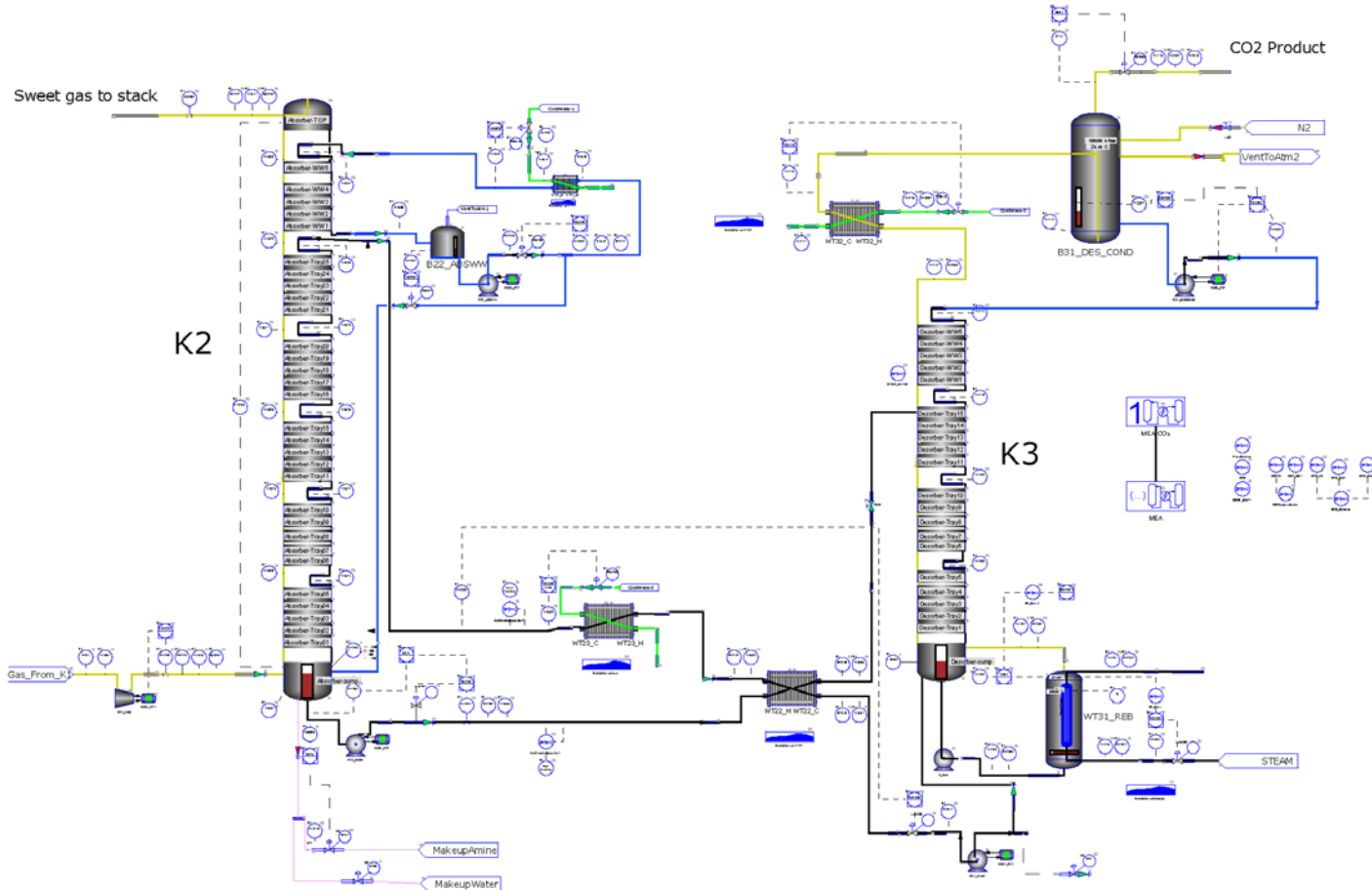
- **The absorber – desorber plant will frequently not be at steady state because of**
  - Various loads at the power plant – Flue gas flow and CO<sub>2</sub> concentration
  - Other disturbances: Steam pressure, plant constraints, weather conditions, solvent degradation, etc
- **Important with good control structures to optimize the plant also under transient periods**
- **First steps for control studies**
  - Provide a good dynamic model of the plant
  - Validate the model with data from the plant

# Dynamic model

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- **Dynamic models of the Brindisi and the Heilbronn plant was developed in WP 11.4 using K-Spice**
- **K-Spice is a general dynamic process simulator from Kongsberg**
  - Extensive experience from oil and gas industries
  - Engineering simulators
  - Operative training simulators
  - Process safety checks
  - Operator procedure verification
- **SINTEF/NTNU needed to:**
  - Set up the process simulation flowsheet with all units and connections.
  - Provide dimensions and design parameters for all process units
  - Implement thermodynamic tables for MEA equilibrium, physical properties
  - Implement control structures, valve characteristics etc.
  - Specify inlet stream specifications and other boundary conditions

# K-SPICE model for the Heilbronn pilot

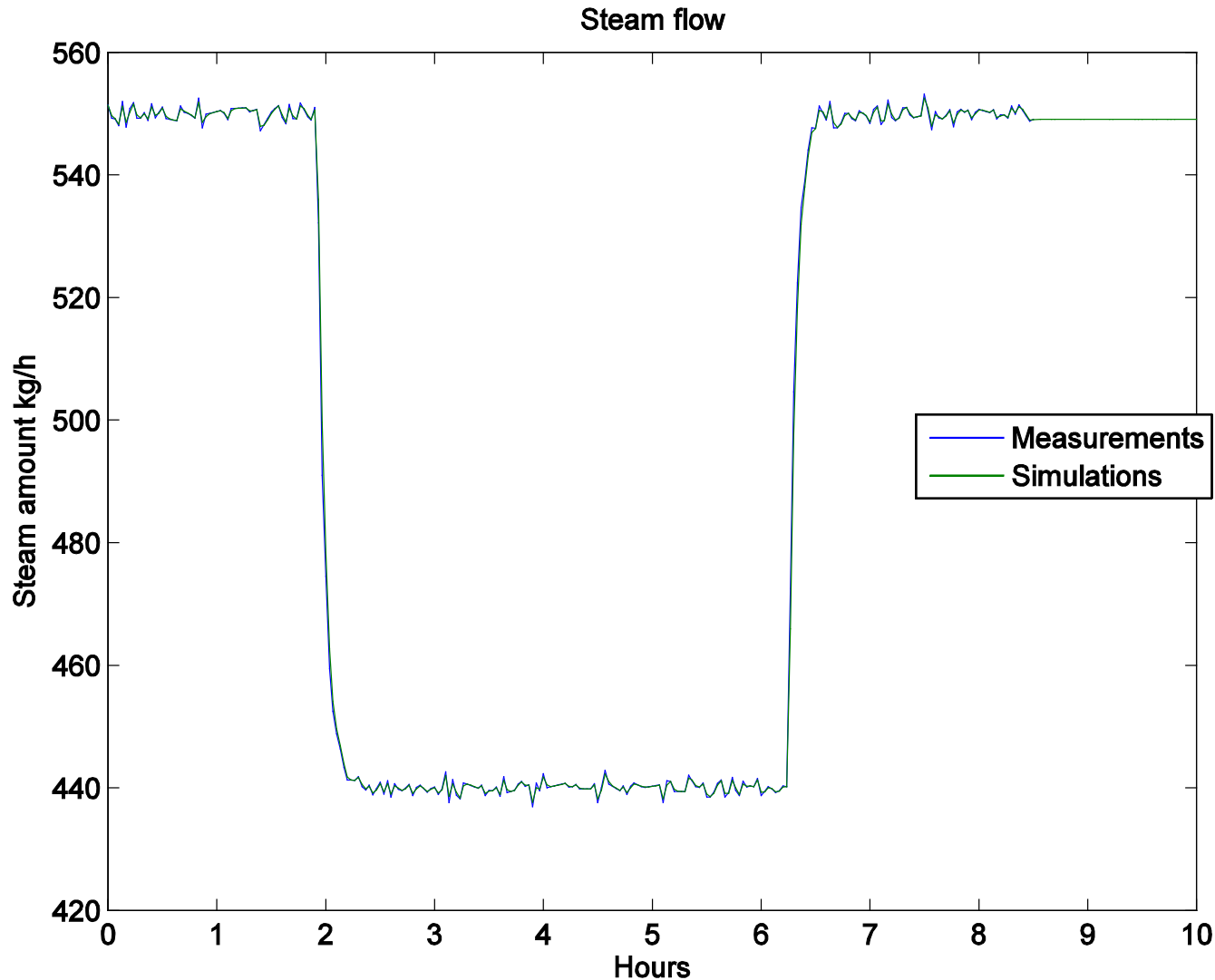


# Tests performed in the campaign

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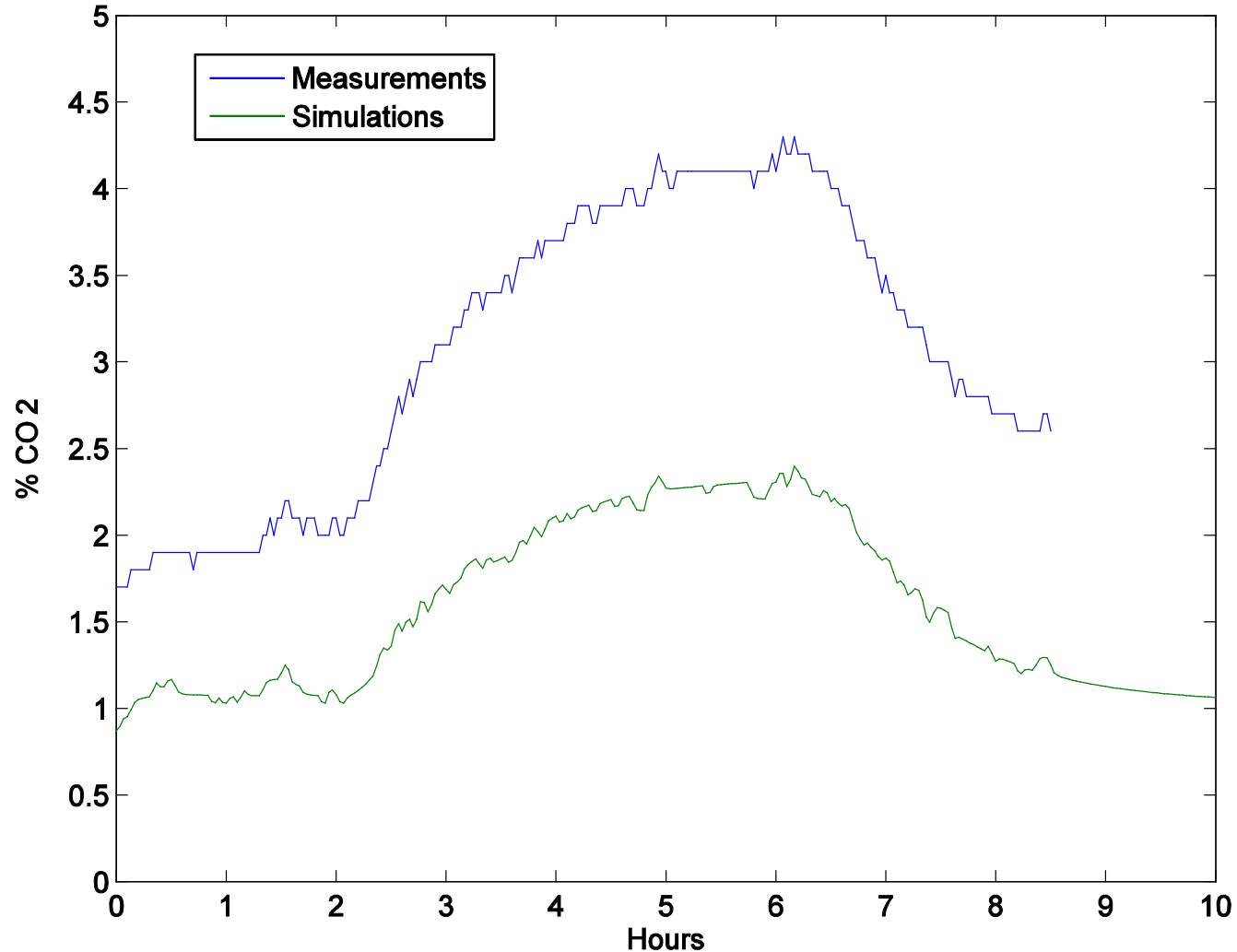
- 1) **Step in reboiler duty at liquid rate 4 m<sup>3</sup>/h**
- 2) **Step in reboiler duty at liquid rate 6 m<sup>3</sup>/h**
- 3) **Step in liquid circulation rate**
- 4) **Step in gas flow**
- 5) **Variation of CO<sub>2</sub> in gas flow**
- 6) **Simultaneous step decrease of gas flow, liquid rate and reboiler duty.**

# Dyn1: Step down in reboiler duty, Liq=4 m<sup>3</sup>/h

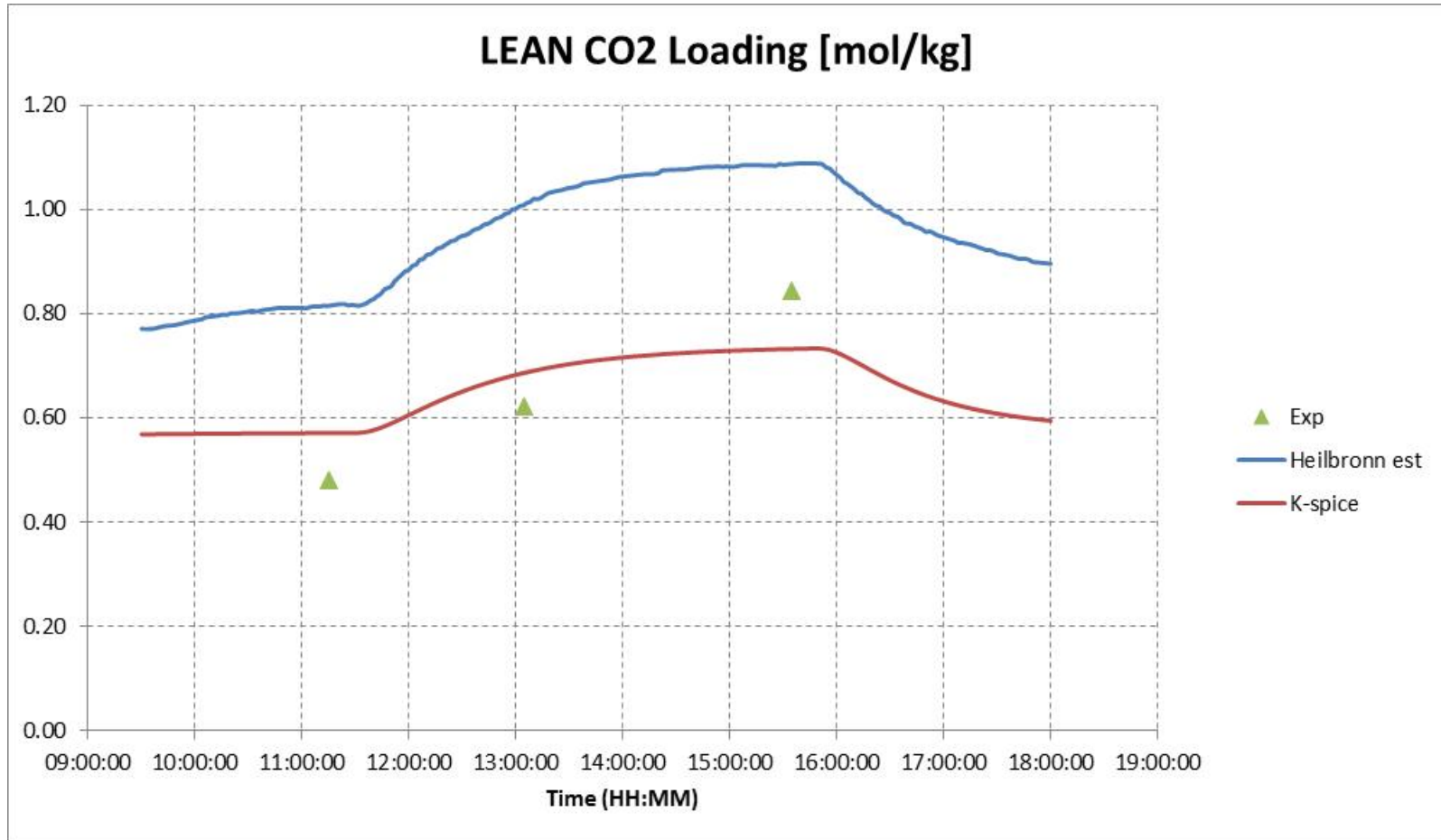


# Dyn1: Step down in reboiler duty, Liq=4 m<sup>3</sup>/h

CO<sub>2</sub> concentration out of absorber

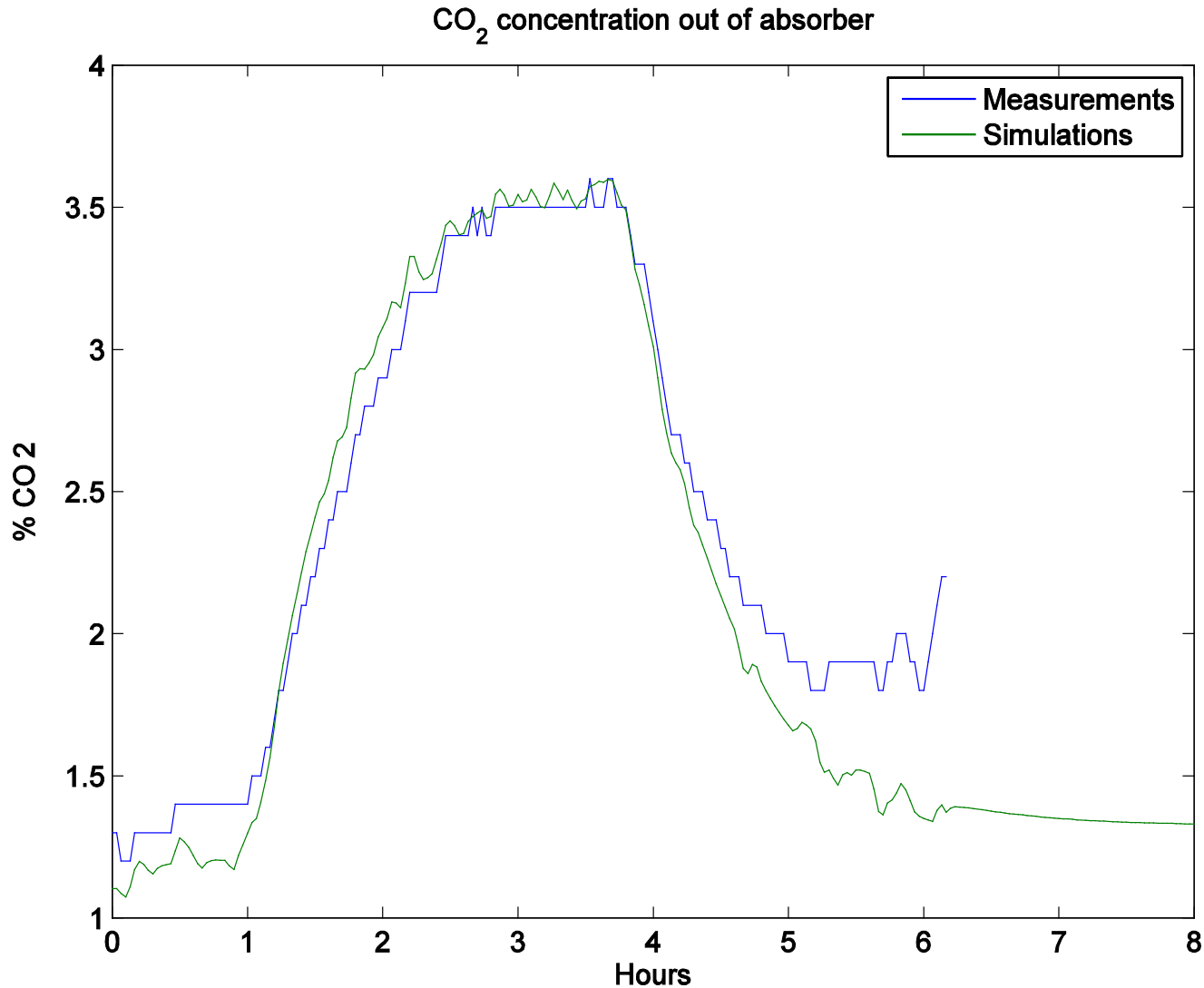


# Dyn1: Step down in reboiler duty, Liq=4 m<sup>3</sup>/h

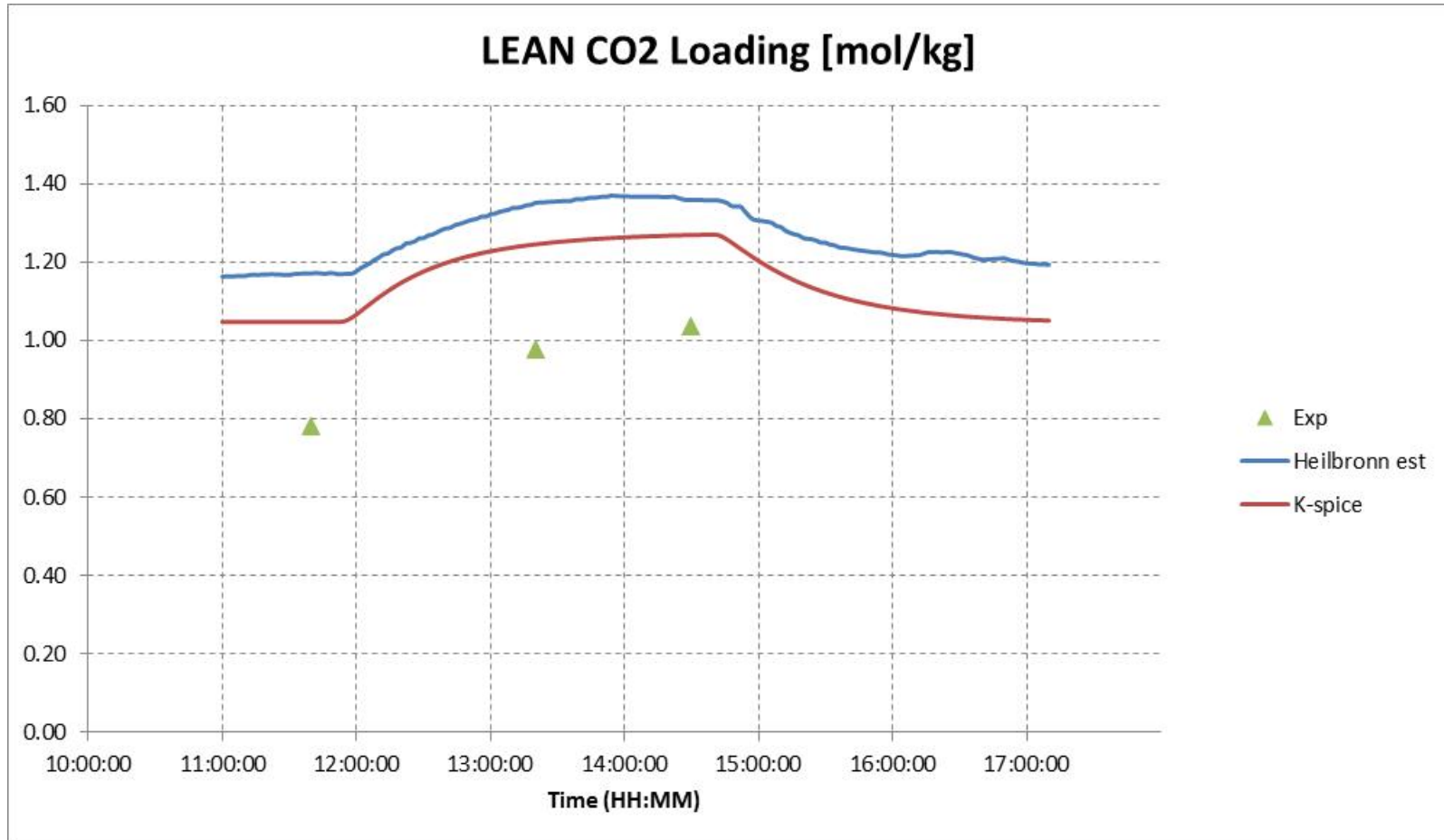




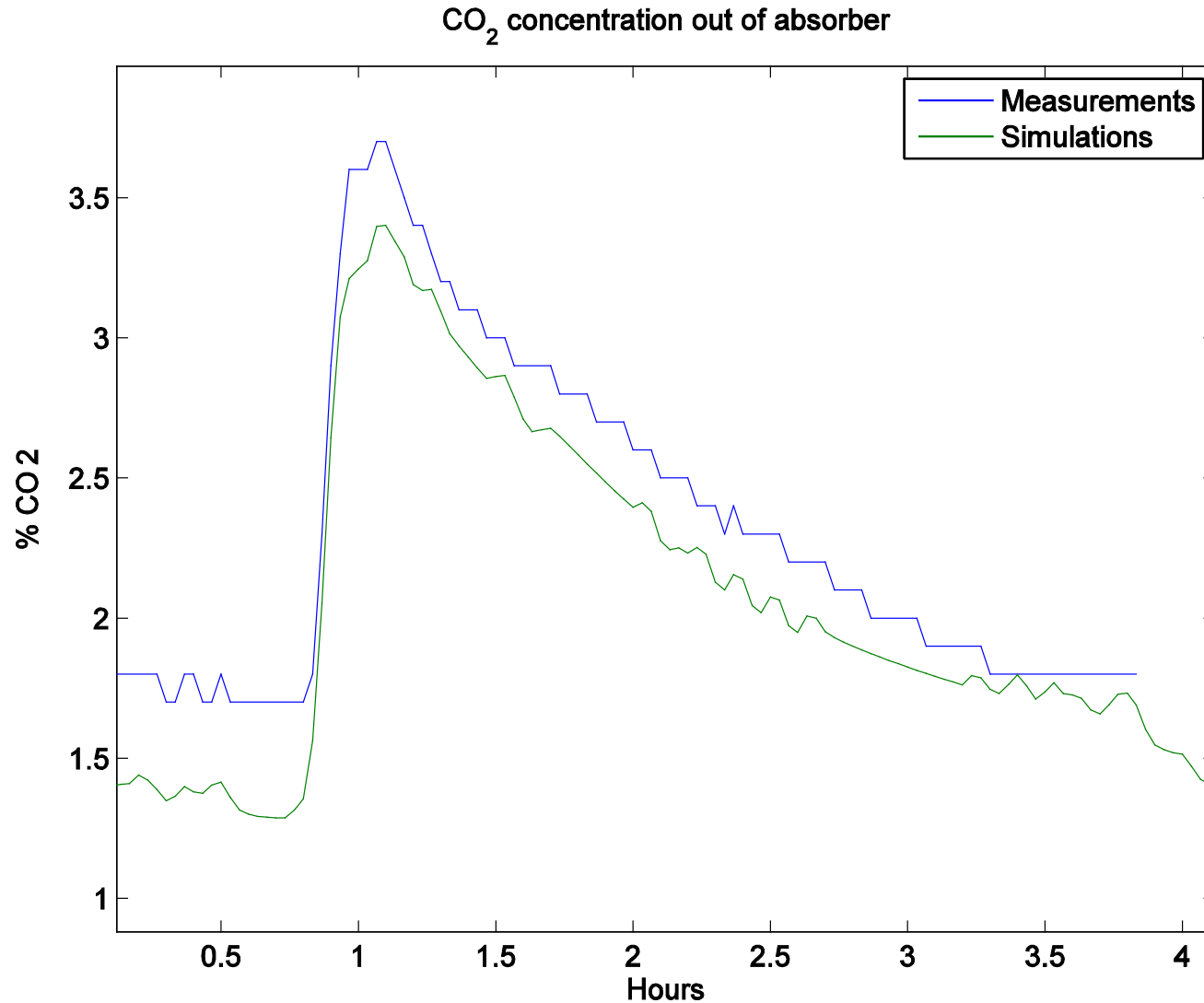
# Dyn2: Step down in reboiler duty, Liq=6 m<sup>3</sup>/h



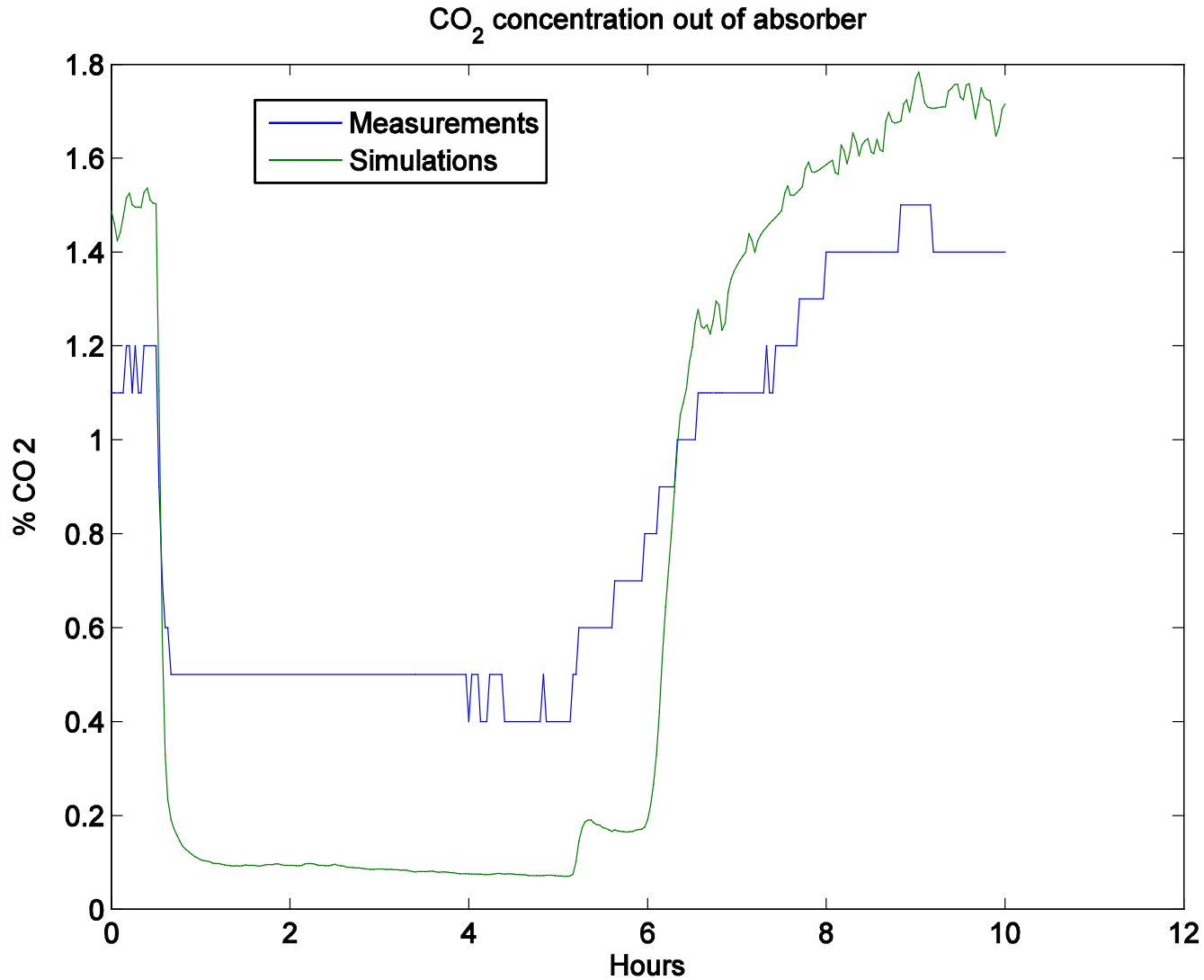
# Dyn2: Step down in reboiler duty, Liq=6 m<sup>3</sup>/h



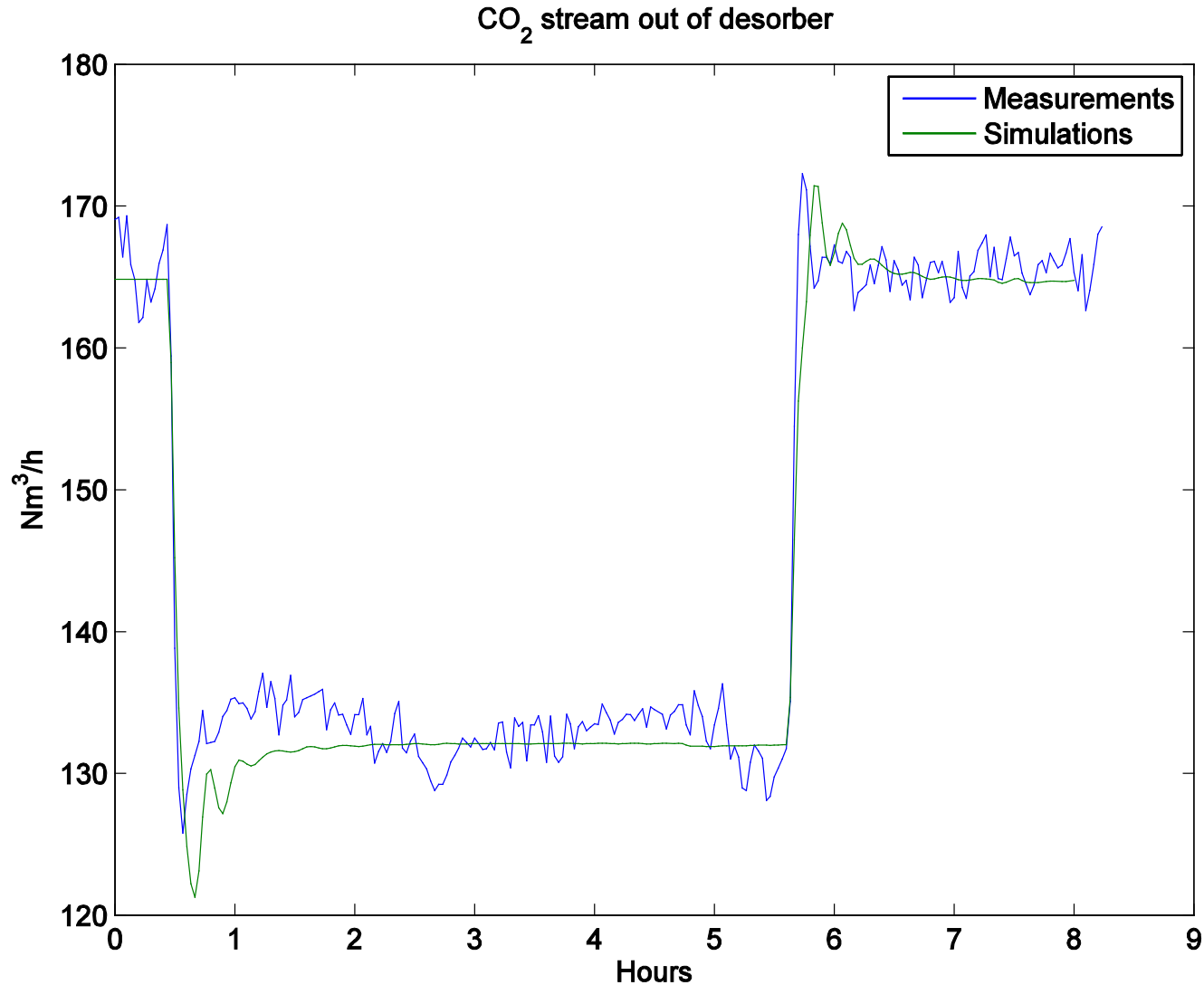
# Dyn3: Step down in solvent flow rate



# Dyn4: Step down in gas flow rate

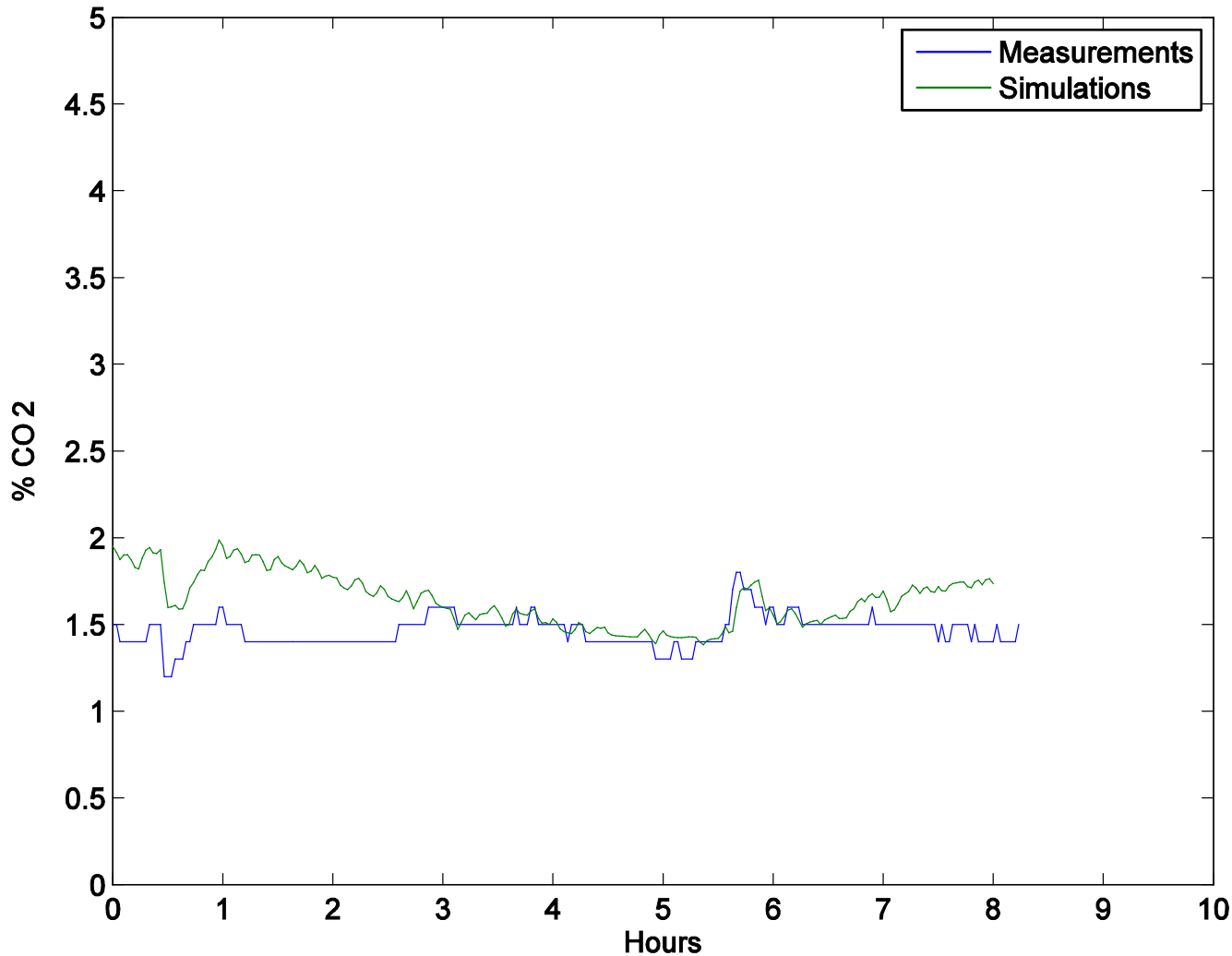


# Dyn6: Simultaneous decrease of flows



# Dyn 6: Simultaneous decrease of flows

CO<sub>2</sub> concentration out of absorber



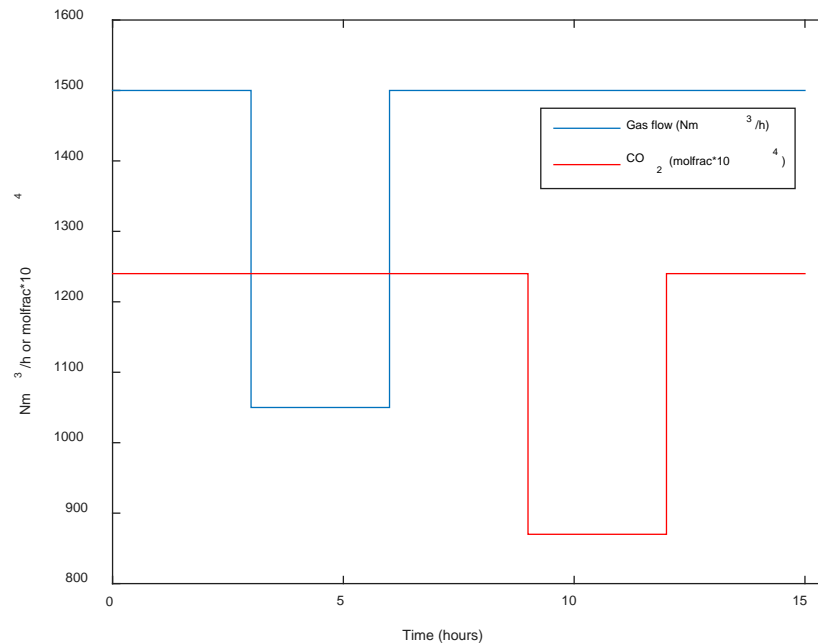
# Summary of the dynamic tests

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- The model is able to capture the process dynamic behavior well.
- Some steady state deviations.
- Almost no changes of the outlet CO<sub>2</sub> concentration when changing all variables with 20%. Ratio control seems to work well.
- Similar dynamic tests was performed at the Brindisi plant. The work was presented at GHGT-12 in Austin, Texas

# Control study

- **Control objectives**
  - 90% capture rate
  - Minimum specific reboiler duty (SRD) in MJ/kg CO<sub>2</sub> captured
- **Testing step changes in flue gas flow and composition**



- **Gas flow rate: 1500 – 1050 Nm<sup>3</sup>**
- **Concentration CO<sub>2</sub>: 12.4% - 8.7%**

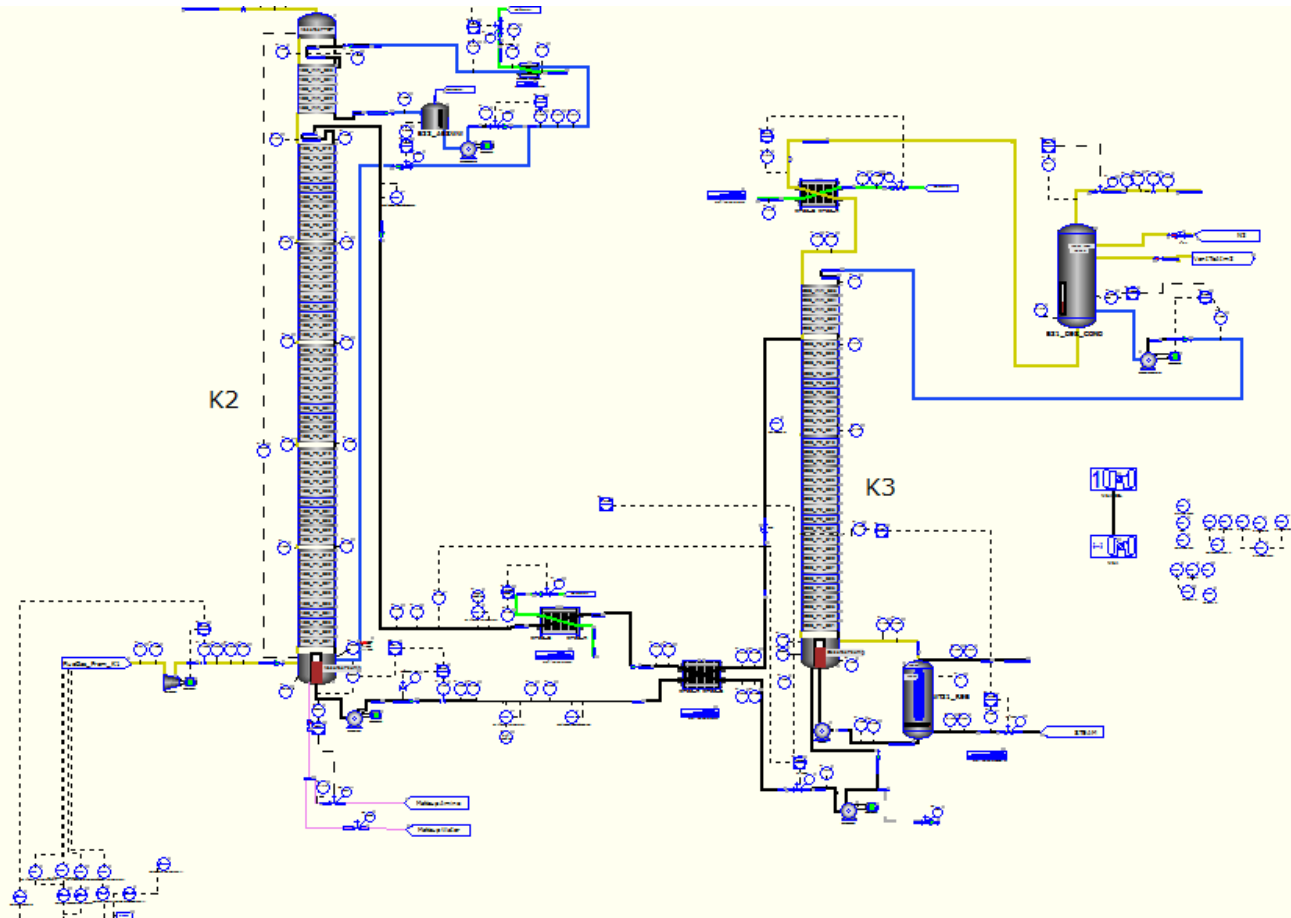


# Two control structures tested

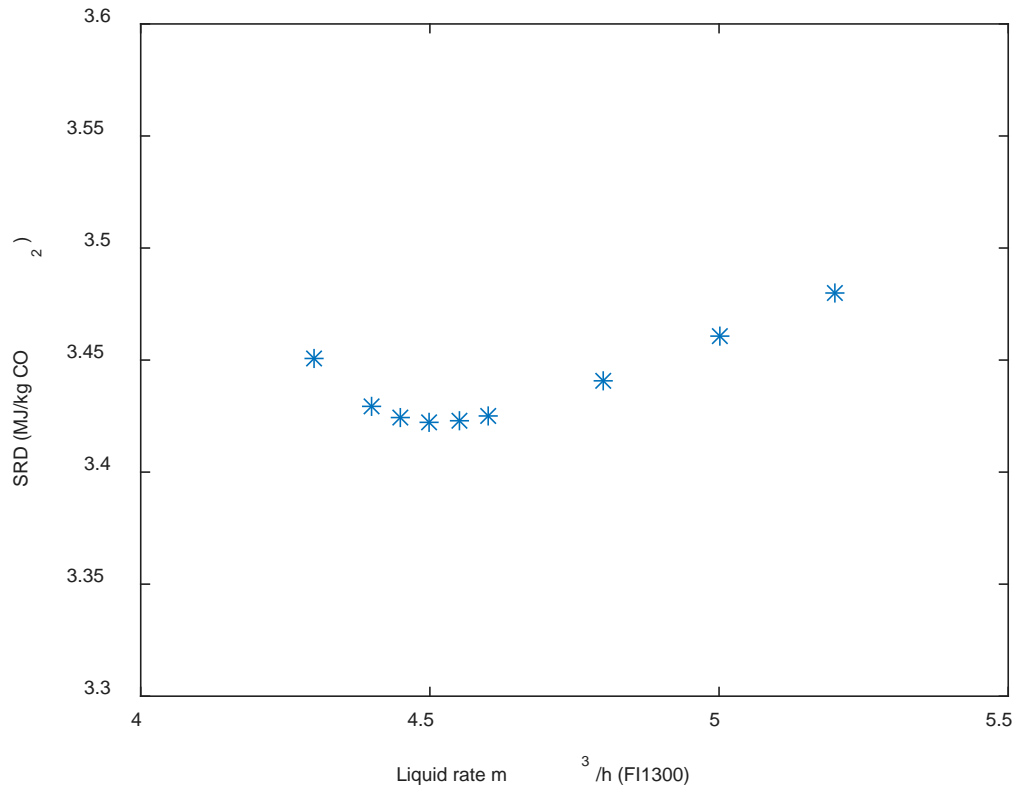
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- **Con1: Use of ratio control (kind of feed forward control) in combination with a slow feed back control on the CO<sub>2</sub> out of the absorber. The control structure is based on the results from the campaign.**
- **Con2: Control of the CO<sub>2</sub> out of absorber by lean liquid rate while keeping a temperature up in the desorber constant. This is a suggestion from the literature by Skogestad et al. on the basis of the "self optimizing control" concept.**
- **Both structures are quite simple to implement**

# K-SPICE model for the Heilbronn pilot

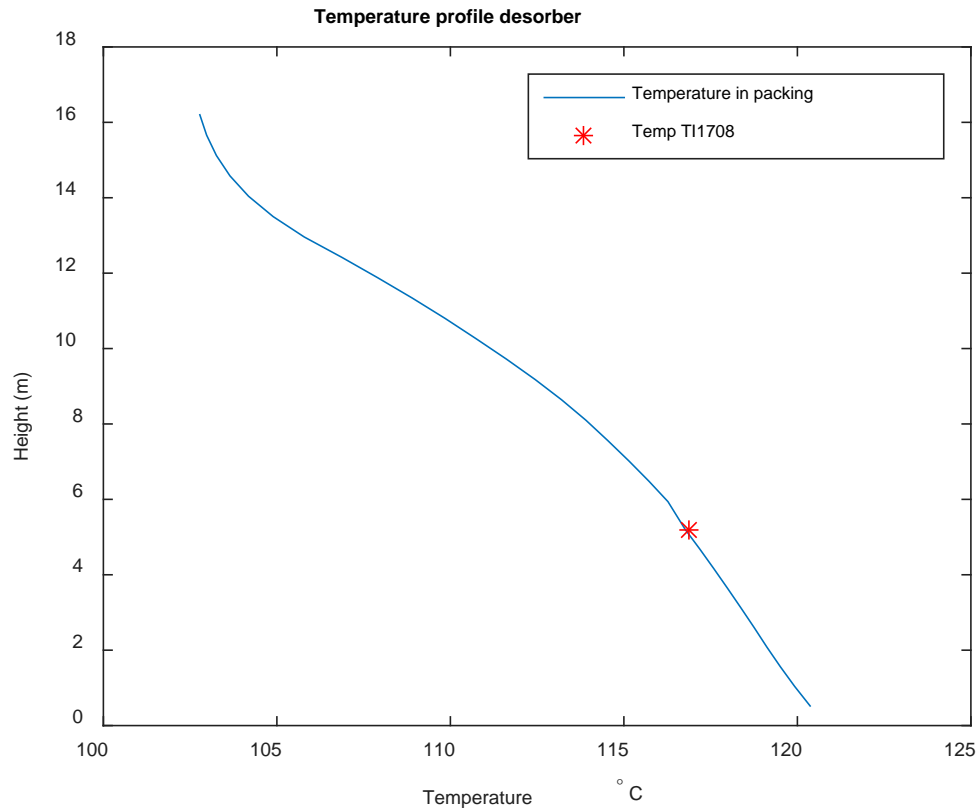


# Optimal steady state as a starting point



All runs 90% capture. Optimal liquid rate 4.5 m<sup>3</sup>/h  
SRD=3.420 MJ/kg CO<sub>2</sub>

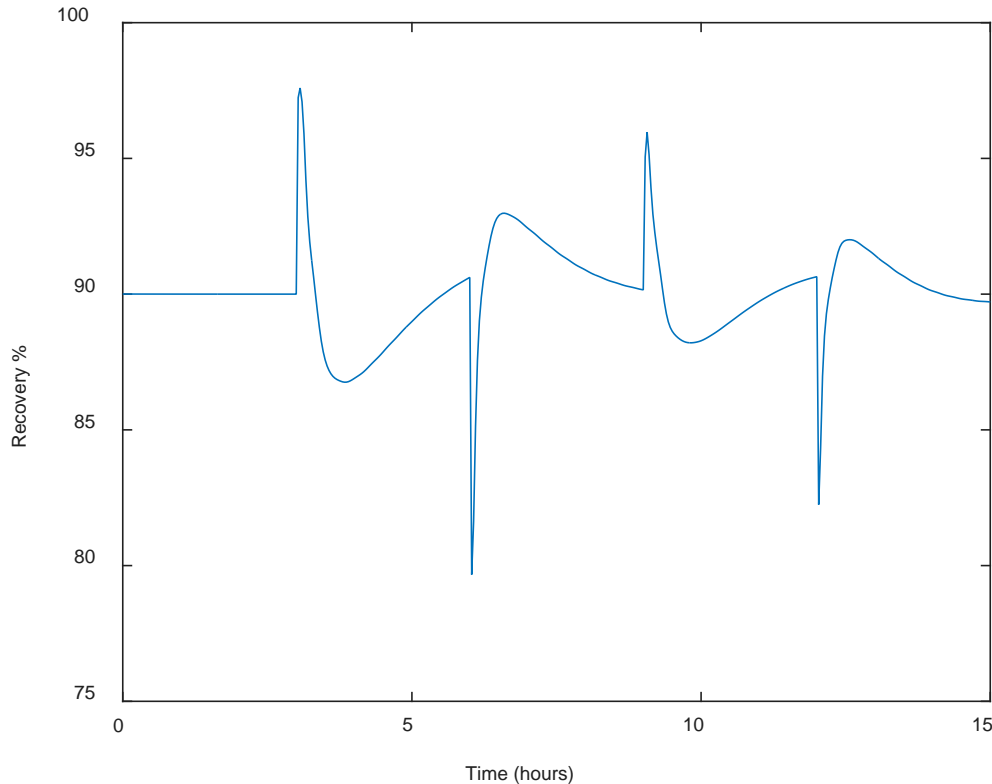
# Optimal steady state point



Temperature profile desorber

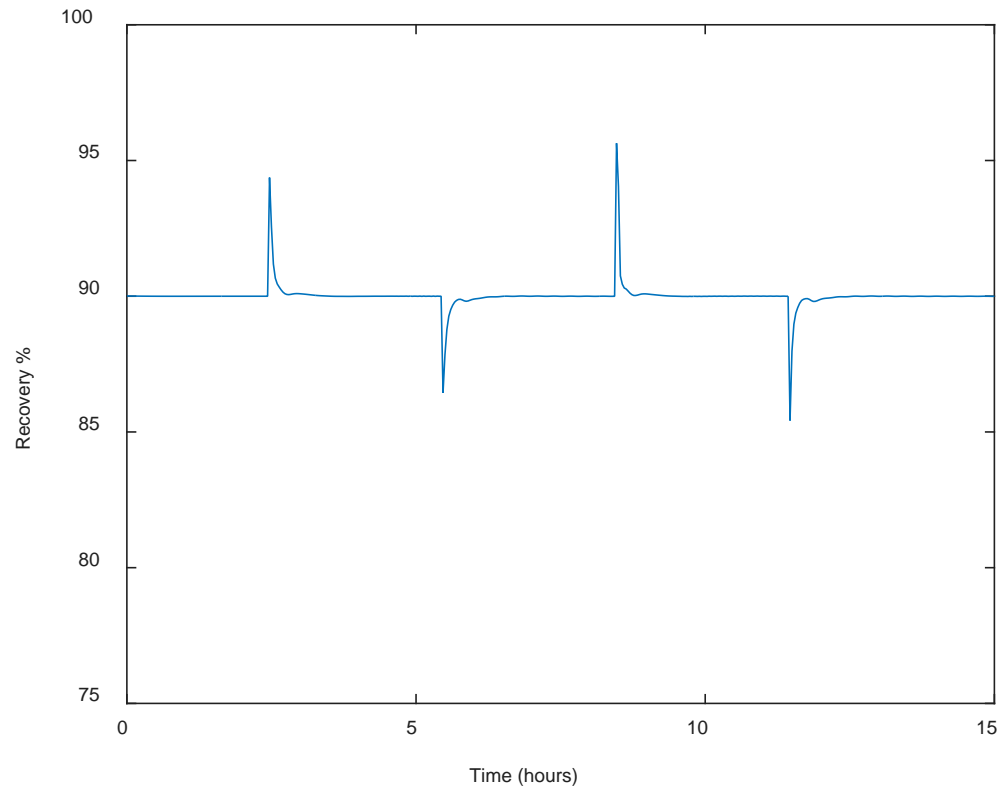
Con2: Keep the T11708 between section 1 and 2 constant

# Result of simulation Con1 (ratio control)



- Reboiler duty and liquid rate proportional to the amount of CO<sub>2</sub> in the flue gas.
- A slow cascade control to keep 90% recovery by reboiler duty .

# Result of simulation Con2



- **Liquid flow to control 90% recovery.**
- **TI1708 in the desorber is kept constant by reboiler duty.**

# Comparison

|       | Recovery % |       | SRD MJ/kg CO <sub>2</sub> |       |
|-------|------------|-------|---------------------------|-------|
|       | mean       | std   | mean                      | std   |
| Con1: | 90.05      | 1.755 | 3.426                     | 0.052 |
| Con2: | 90.00      | 0.521 | 3.420                     | 0.077 |

- **The mean value for recovery and SRD very similar for Con1 and Con2 and the optimal steady state case.**
- **Tighter control of the recovery with Con2**
- **Con2 should be preferred.**

# Summary

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- A dynamic model of the Heilbronn plant was implemented in K-Spice and tested against step responses at the plant.
- In spite of some steady state deviations, the model was able to capture the process dynamics very well.
- One may therefore assume that dynamic studies using the model will be representative for the plant.
- The plant was simulated for 15 hours with 30% steps in gas flow rate and CO<sub>2</sub> concentrations.
- The average specific reboiler duty (SRD in MJ/kg CO<sub>2</sub>) over the time frame was similar and close to optimal
- However, the Con2 showed tighter control of the recovery and should be preferred.